

# METAL OXIDE VARISTORS

## Zinc Oxide Voltage Dependent Resistor U.L. File #E98144 VDE File #14480-4790-1001/A1F

### DESCRIPTION

#### GENERAL

V(oltage) D(ependent) R(esistor)—varistors—have a high degree of non-linearity between resistance value and applied voltage. This characteristic is created by non-homogeneous metal oxide materials selected for rectifying action at the interface of two crystals. The electrical characteristic of the component is the product of a large number of these interstitial junctions, forming a complex network of series and parallel rectifying junctions.

The Philips Components product line uses ZnO (with doping) as the element material. ZnO offers much sharper V-I curves than other commonly used materials.

#### PHYSICAL

A disc of low beta metal oxide ceramic with two solid tinned copper wires. ZnO's are epoxy coated.

**ELECTRICAL DATA**, see also Table 1 and subsequent curves.

Climatic category	40/125/56
Insulation voltage	2500 V
Temperature coefficient of voltage at 1 mA	-0.065%/°C
Derating (see Fig. 31.)	

#### Mounting

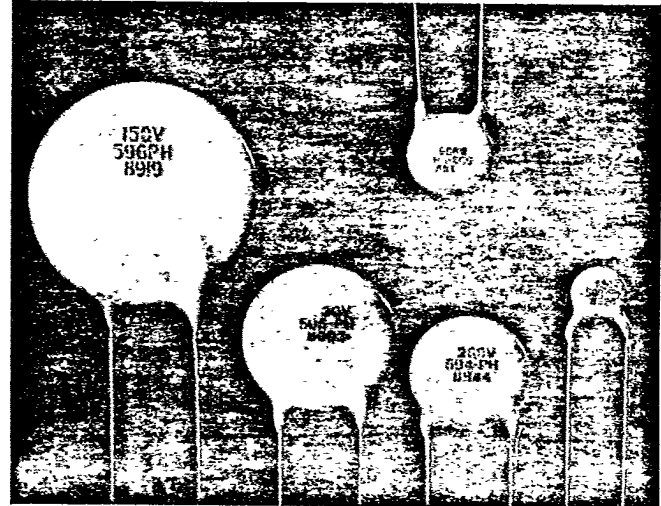
Series 592 thru 595 available on	Tape & Reel.
Series 592 and 593 available on	Ammo Pack

#### Soldering

Solderability	max. 240°C, max. 4s
Resistance to heat	max. 265°C, max. 11s

#### Impact

free fall	39.4" (1000 mm)
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#### Termination Strength

Tensile strength	2.25 lb (10 N)
Bending	1.12 lb ( 5 N)

Flammability	Nonflammable
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Non-Linear Resistors

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## INTRODUCTION TO METAL OXIDE VARISTORS

Metal Oxide Varistors, also called V(oltage) D(ependent) R(esistors), show a high degree of non-linearity between their resistance value and the applied voltage. They are made of non-homogeneous material giving a rectifying action at the contact of two particles. The electrical characteristic of the conglomeration is determined by a large number of crystal contacts which form a complicated network of series and parallel rectifying contacts.

These resistors have found a diversity of applications in the different sectors of electronics. They offer an inexpensive and reliable solution for protection of electronic circuits, semiconductor components, collectors of motors, relay contacts, etc. against over-voltages and their consequences.

## MANUFACTURING PROCESS

Crystals of metal oxides, with the right electrical and dimensional properties are pressed together with a ceramic binder to the shape of discs. After a drying period the varistors are sintered at a high temperature. Firing time, temperature and gaseous atmosphere have an important influence on the electrical characteristics. The contacts are metallized with silver enabling good electrical contact. After leads have been soldered to the contacts the varistors are epoxied and laser marked.

During and after the manufacturing process the electrical properties are controlled not only to ensure that the varistors are within the specification but also to control stability and reliability.

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## ELECTRICAL PROPERTIES

### Direct Current

The relation between voltage and current of a varistor can be approximated by:

$$V = C I^\beta$$

where  $V$  is the voltage in volts,  $I$  the current in amperes and  $C$  and  $\beta$  are constants. This equation is illustrated in Fig. 1. In principle the same characteristic is plotted for a specific type on a double logarithmic scale in Fig. 2. For not too small values of current this relation is a straight line which follows directly from the equation  $\log V = \log C + \beta \log I$ . In this case  $\beta$  is the directional coefficient of the straight line.

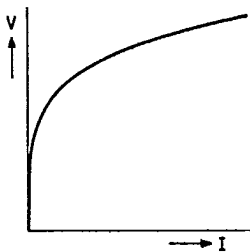


Fig. 1 Shape of the voltage/current characteristic of a varistor when plotted on a linear scale.

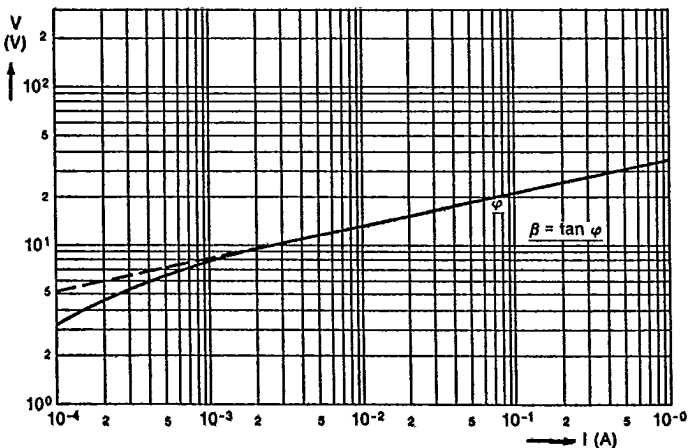


Fig. 2 Voltage/current characteristic of a varistor plotted on a logarithmic scale.

In order to determine the exact values of the constants  $C$  and  $\beta$  it is necessary to measure three points of the characteristic. Only when these are on a straight line when plotted on a double logarithmic scale, is extrapolation permit-

ted (only to higher values). Equation (1) may also be written:

$$I = \left(\frac{V}{C}\right)^\alpha \quad (2)$$

in which:

$$\alpha = 1/\beta \quad (3a)$$

and

$$K = \frac{1}{C^{1/\beta}} = \frac{1}{C^\alpha} \quad (3b)$$

The varistors do not have a polar effect; this means that when the voltage is changed from positive to negative, the current changes its direction, but retains its value. Strictly speaking, Eqs (1) and (2) are valid only when the absolute values are taken for  $I$  and  $V$ . In a.c. calculations this may be very important. For practical design, reference is made to the voltage/current characteristics given in the data sheets of the relevant varistor types.

### Practical values and specification

The  $C$  and  $\beta$ -values of varistors depend on the composition of the material and on the method used in the processing; furthermore, the  $C$ -value depends on the shape and the dimensions of the varistor. Practical  $\beta$ -values are  $\beta = 0.02$  to  $0.035$ .

It is inherent to the material properties that the  $\beta$ -value of a varistor with a low  $C$ -value will always be higher than that of a varistor with a high  $C$ -value. Practical  $C$ -values range from 14 to a few thousand. As the method of fabrication compels a minimum thickness and, as will be seen further, enlarging of the surface area gives little change in the  $C$ -value, the latter has for practical reasons a limited lowest value.

According to Eq. (1) it is possible to specify the electrical characteristics of a varistor by giving its  $C$  and  $\beta$ -values. The advantage of this specification is that only two parameters are used. The disadvantage is, however, that due to the inevitable tolerances on the  $\beta$ -values, the spread in voltages at low currents (in the working area) becomes very large. It is for this reason that the method of specifying by the  $C$ -value defined at 1 A is abandoned and we now specify the voltage across the varistor at currents which lie in the working area (1, 10 or 100 mA instead of 1 A). In this way it is possible to supply varistors which have much closer tolerances in the area where they are used, see Fig. 5.



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## Varistors in series

For each varistor we can write the equation:

$$V = C\beta. \quad (1)$$

When  $n$  equal elements are connected in series and a voltage of  $n$  times the original voltage is applied, the current will be the same as for  $V$  volts over one varistor. Consequently we may write for a series circuit of  $n$  varistors:

$$nV = C'\beta. \quad (4)$$

From Eqs (1) and (4) it is evident that,

$$C' = nC, \quad (5)$$

which means that the  $C$ -value of a varistor can be increased by series connection.

## Varistors in parallel

For one varistor again we have:

$$V = C\beta. \quad (1)$$

When  $n$  of these varistors are connected in parallel and the same voltage  $V$  is applied, the current in each varistor will still be the same. The total current in the circuit will be  $nI$ . This gives the following equation:

$$V = C''(nI)\beta. \quad (6)$$

From Eqs (1) and (6) it follows:

$$C'' = \frac{C}{n\beta} \quad (7)$$

As varistors have a  $\beta$ -value from 0.02 to 0.40, it is clear that the  $C$ -value will decrease very little by connecting two or more elements in parallel. When, e.g.  $\beta = 0.20$ , 32 varistors are needed for a 50% reduction of the  $C$ -value. It is important that in parallel circuits all varistors have about the same  $\beta$  and  $C$ -values, otherwise the current division will very much depend on the voltage across the circuit.

**Note:** On no occasion may a varistor be connected in parallel with the aim of obtaining higher power dissipation.

## Resistance value

When defining  $R$  as usual as the quotient of voltage and current, we find:

$$R = \frac{V}{I} = \frac{C\beta}{I} = \frac{C}{I^{1-\beta}} \quad (8)$$

or when starting from the form  $I = \left(\frac{V}{C}\right)^\alpha$ :

$$R = \frac{V}{I} = \frac{V}{\frac{V^\alpha}{C^\alpha}} = \frac{C^\alpha}{V^{\alpha-1}} \quad (9)$$

From these equations it is once more evident that the resistance value is not a constant one,

but is very much dependent on the values of voltage and current.

## Dissipated power

The power dissipated in a varistor is equal to the product of voltage and current, so it may be written:

$$W = IV = \left(\frac{V}{C}\right)^\alpha \cdot V = \frac{V^{\alpha+1}}{C^\alpha} \quad (10)$$

When the coefficient  $\alpha = 5$ , the power dissipated by the varistor is proportional to the 6th power of the voltage. A voltage increase of only 12% will, in this case, double the dissipated power. Consequently it is very important that the applied voltage does not rise above a certain maximum value, as otherwise the permissible rating will be exceeded.

In addition, since varistors have a negative temperature coefficient, at higher dissipation (and accordingly higher temperature) the resistance value will decrease and the dissipated power will increase still more.

## Temperature coefficient

In the foregoing formulae no temperature effects have been taken into account. These, however, may not always be neglected, as the  $C$ -value has an appreciable negative temperature coefficient. The  $\beta$ -value is practically independent of the temperature. With good approximation it may be written:

$$C_t = C_0 (1 + at), \quad (11)$$

in which:

$C_t$  =  $C$ -value of the varistor at  $t$  °C;  
 $C_0$  =  $C$ -value of the varistor at 0 °C;  
 $a$  = temperature coefficient.

For different materials the value of  $a$  lies between  $-0.0010$  and  $-0.0018$ . Thus, for circuits where the current is constant, the temperature coefficient on voltage lies between  $-0.10$  and  $-0.18\%$  per degree C.

For circuits where the voltage is constant the temperature coefficient on current lies between  $+0.4$  and  $+0.8\%$  per degree C, depending on the  $\beta$ -value.

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## High frequency alternating current

For low frequencies the small capacitance of the varistor does not affect the voltage dependency of the resistance. For high frequencies, however, this parallel capacitance may not be neglected. For low voltages and currents they may even determine the impedance of the varistor. At high voltages, the influence of the capacitance is less serious; because in that case the resistance over which this capacitance is shunted has decreased. In general the effect of the capacitance in h.f. circuits will be an apparent increase of  $\beta$ . Furthermore the voltage/current graph on a logarithmic scale will no longer be a straight line.

A number of curves demonstrating this effect are given in Fig. 3.

## PERMISSIBLE DISSIPATION

The temperature which a varistor will reach is determined by the dissipated power, the heat conductivity of the material, the contact with, and the nature of, the surrounding medium and by the ambient temperature. As already explained the dissipated power will increase rapidly with increasing voltage.

The cooling per degree Celsius, though increasing slightly with temperature, depends mainly on the total surface area of the varistor.

For most varistor types the maximum permissible body temperature is 125°C.

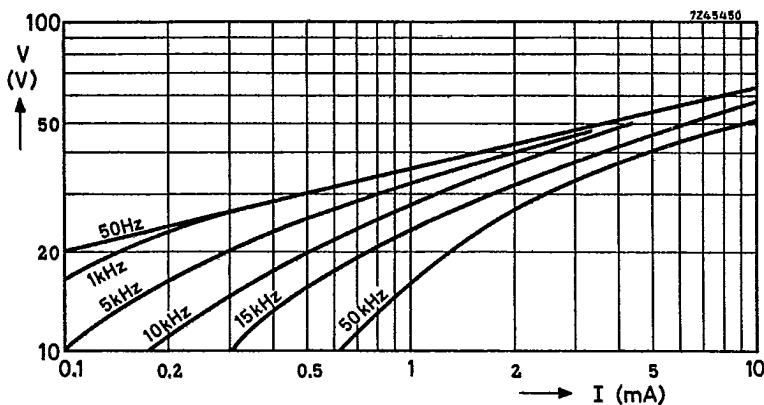


Fig. 3 Voltage/current relation for different frequencies.



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## ZINC-OXIDE VOLTAGE DEPENDENT RESISTORS

Unlike SiC types, the ZnO varistors are mainly intended for applications requiring intermittent power dissipation, i.e. transient suppression and contact arc prevention. In their transient suppression role, the symmetrical mode of operation allows them to be connected directly across a.c. power lines carrying r.m.s. voltages. They are capable of withstanding voltage or current pulses with a high peak energy level. A typical  $\beta$  for this type of varistor is 0.03. This means that, if the current through the varistor increases by a factor of 10 within the straight-line portion of the characteristic, the voltage across it increases by a factor of 1.07.

A typical V/I characteristic for one of these varistors is shown in Fig. 4. The upward turn of the characteristic (decreasing non-linearity) is due to the increasing influence of the linear series resistance of the component as its non-linear resistance falls to very low values at extreme currents. A good approximation of the relationship between the voltage and the current in the curved portion of the characteristics is given by the expression:

$$V = CI\beta + IR_S$$

where  $R_S$  is the series resistance of the varistor.

## Normal operating conditions of the ZnO varistor

Owing to the extreme nonlinearity of the voltage/current characteristic of ZnO varistors, and the necessity to allow a margin for the extra dissipation during a transient, ensure that the maximum voltage applied across the varistor during normal operation never attains such a value that the specified average dissipation limit of the varistor is approached. This will never be a problem if the varistor is selected according to the figures for max. r.m.s. voltage in the data sheet. The peak value of the sinusoidal voltage applied to the varistor must always be less than the minimum voltage specified at 1 mA. If the applied voltage is other than sinusoidal, the varistor should be selected on the basis of the specified maximum peak working voltage.

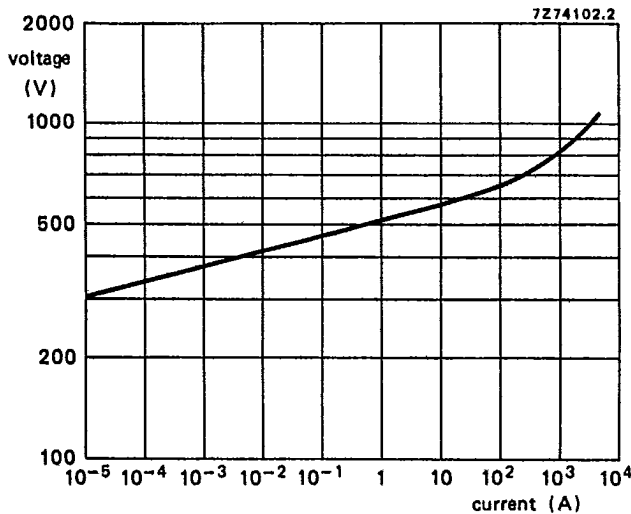


Fig. 4 Typical V/I characteristic of ZnO varistor 2322 595 52516 for 220 V mains supply.

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## HOW TO MEASURE VARISTORS

The following points have to be considered when measuring varistors.

1. Use only d.c. voltage.
2. Keep the measuring time as short as possible. Self-heating effects may influence the measurements due to the negative temperature coefficient of the varistors.
3. When the varistors are specified at a voltage and current which is above the maximum dissipation, pulses should be used. For instance all zinc oxide types, which are for spike/transient suppression are measured under pulse-conditions. These types are measured with a standard pulse current 8/20  $\mu$ s as defined in IEC 60-2, section 6.
4. The  $\beta$ -value measurement needs some explanation. As mentioned earlier the  $\beta$ -value is not always constant but depends on the voltage and current. The  $\beta$ -values of our discs are measured between 0.3 I and 3 I, where I is the current at which the varistor is specified. For example:

$$\beta = \log \frac{V_2}{V_1}; \text{ with } V_2 = \text{voltage at } 3 I, \\ V_1 = \text{voltage at } 0,3 I.$$

## TOLERANCES

Standard varistors are specified with a certain tolerance on voltage and a spread on  $\beta$ -value. It can be seen in Fig. 5 that due to the spread in  $\beta$ -value the tolerance on voltage may increase at currents other than the specified current at which the varistor is measured.

For some applications, where tolerances have to be kept as low as possible, the varistors are measured at a current or voltage which lies near to its working point in the circuit. For other applications, especially spark suppression, it is often important to specify the varistor at two points: a point at low current or low voltage and a point at high current or high voltage.

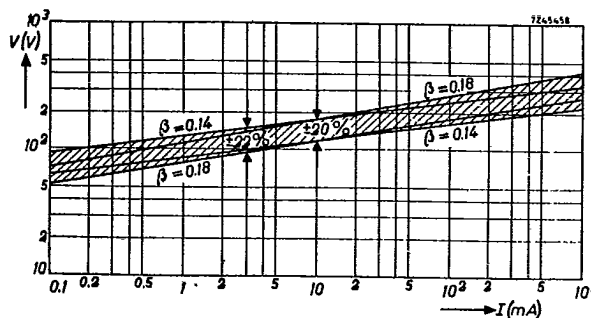


Fig. 5 Spread of voltage/current characteristic due to  $\beta$ -tolerance.





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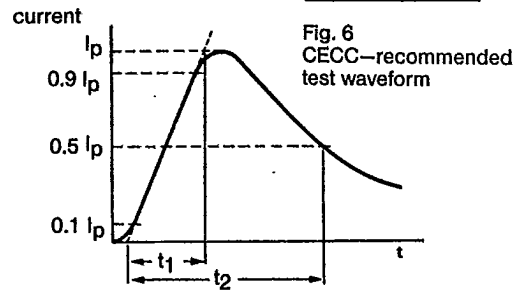
## Electrical characteristics

Varistor characteristics are measured at high currents and high energy levels using an exponentially decaying waveform, as shown in Fig. 6, representative of lightning surges and the discharge of stored energy in reactive circuits. Based on CECC recommendations, the standard waveform used for current and voltage rating measurements has a virtual front duration of  $8\mu\text{s}$  and an impulse duration of  $20\mu\text{s}$ . It is therefore called the  $8/20\mu$  waveform.

For energy rating measurements, a longer duration waveform (the  $10/1000\mu\text{s}$  waveform) having exactly the same format as Fig. 6 is used.

Voltage-current characteristics for each varistor series are shown in Figs. 7 to 20.

$t_1$	$t_2$
$8\mu\text{s}$	$20\mu\text{s}$
$10\mu\text{s}$	$1000\mu\text{s}$



592 SERIES (A)

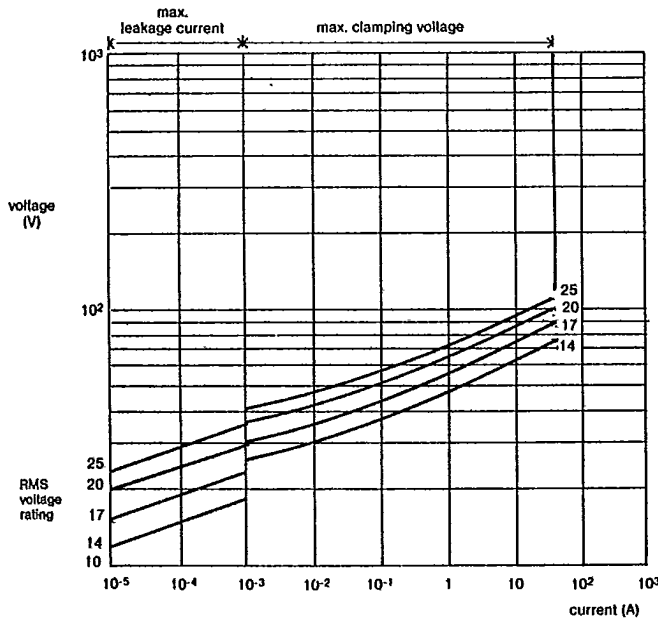


Fig. 7  
V-I characteristics, 592 series, 14 to 25 V

592 SERIES (B)

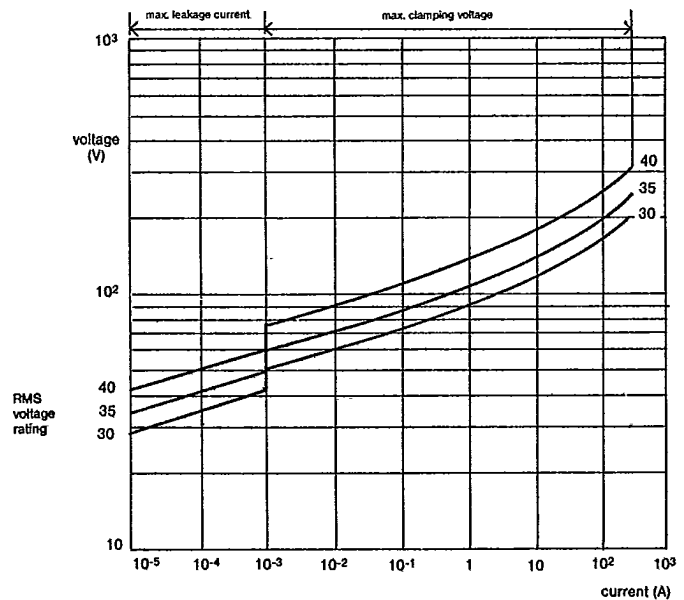


Fig. 8  
V-I characteristics, 592 series, 30 to 40 V

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## Zinc Oxide Disc

### 592 SERIES (C)

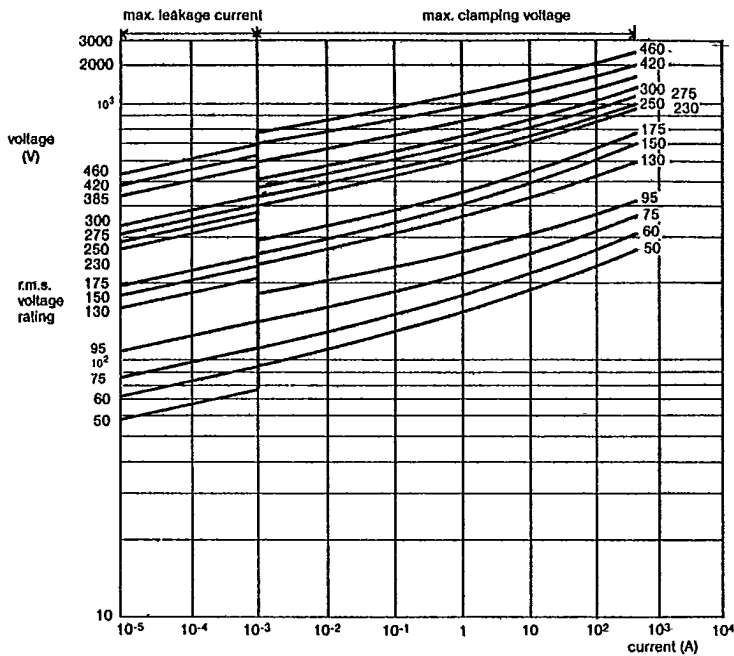


Fig. 9  
V-I characteristics, 592 series, 50 to 460 V

### 593 SERIES (A)

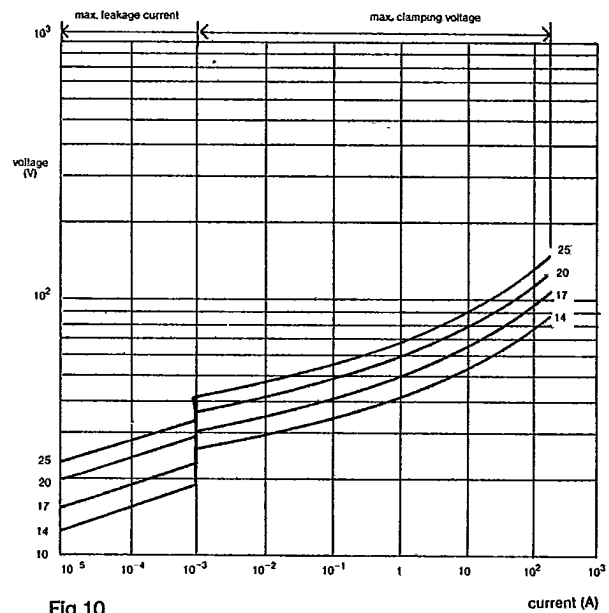


Fig. 10  
V-I characteristics, 593 series, 14 to 25 V

### 593 SERIES (B)

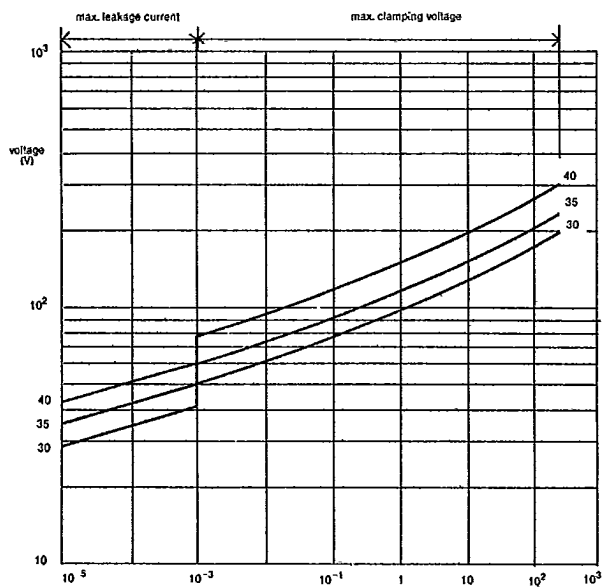


Fig. 11  
V-I characteristics, 593 series, 30 to 40 V

### 593 SERIES (C)

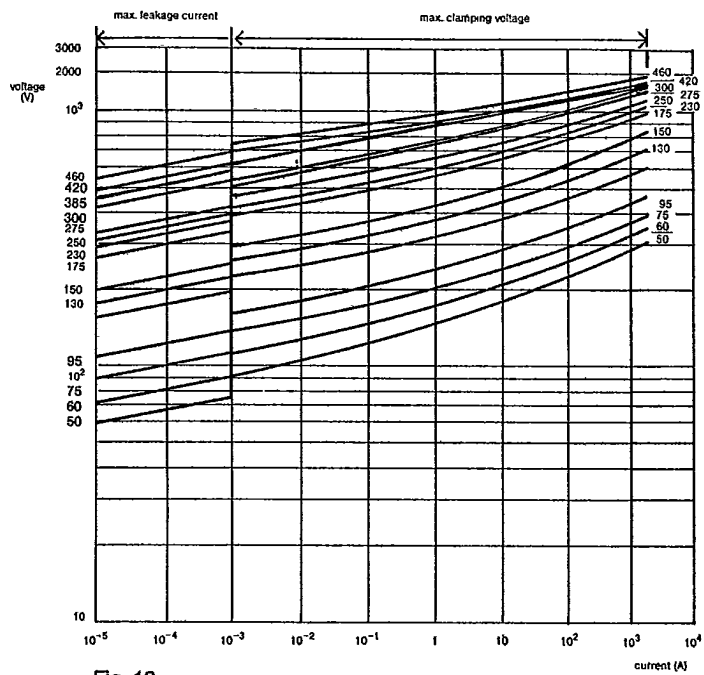


Fig. 12  
V-I characteristics, 593 series, 50 to 460 V

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# METAL OXIDE VARISTORS

## Zinc Oxide Disc

### 594 SERIES (A)

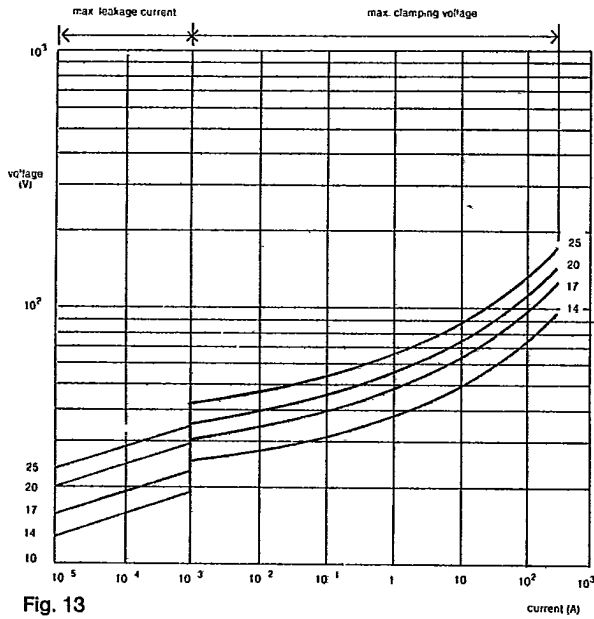


Fig. 13  
V-I characteristics, 594 series, 14 to 25 V

### 594 SERIES (B)

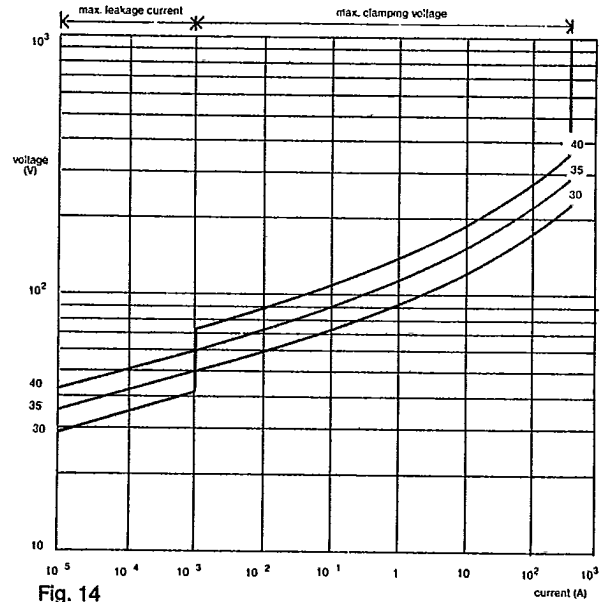


Fig. 14  
V-I characteristics, 594 series, 30 to 40 V

### 594 SERIES (C)

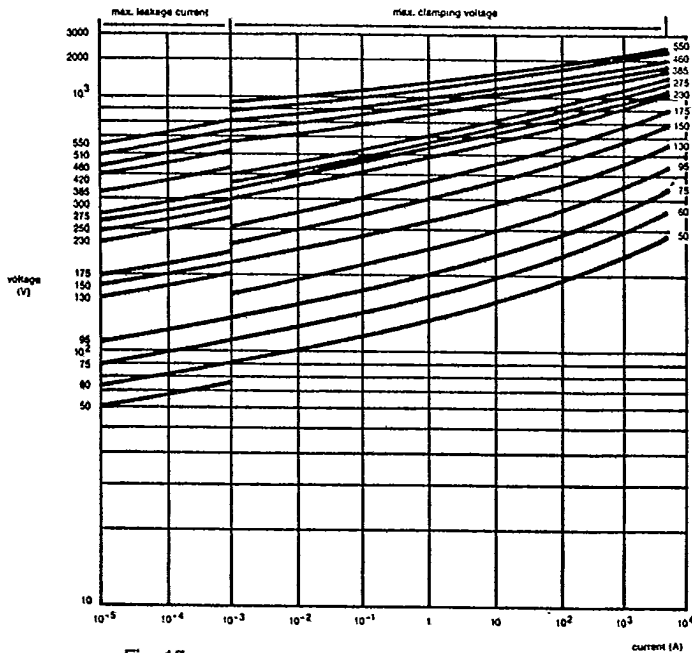


Fig. 15  
V-I characteristics, 594 series, 50 to 550 V

### 595 SERIES (A)

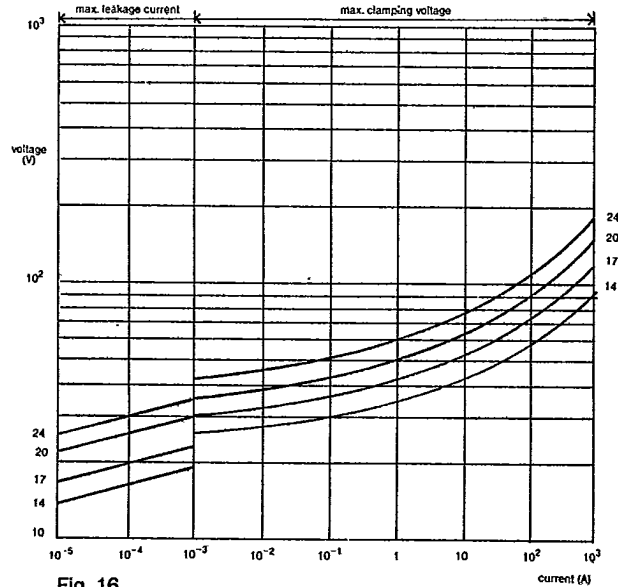


Fig. 16  
V-I characteristics, 595 series, 14 to 25 V

# METAL OXIDE VARISTORS

## Zinc Oxide Disc

### 595 SERIES (B)

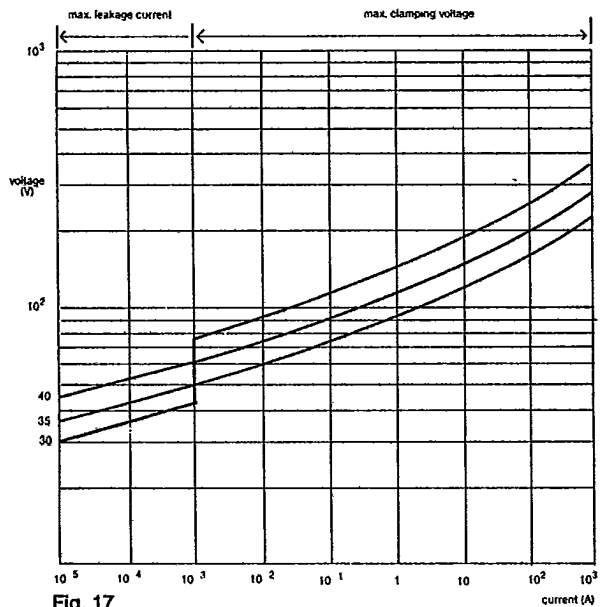


Fig. 17  
V-I characteristics, 595 series, 30 to 40 V

### 595 SERIES (C)

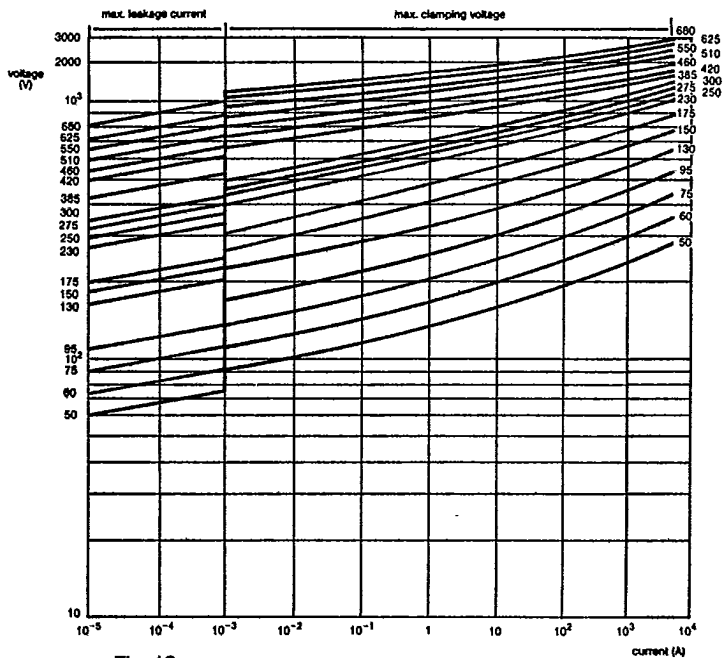


Fig. 18  
V-I characteristics, 595 series, 50 to 550 V

### 596 SERIES (A)

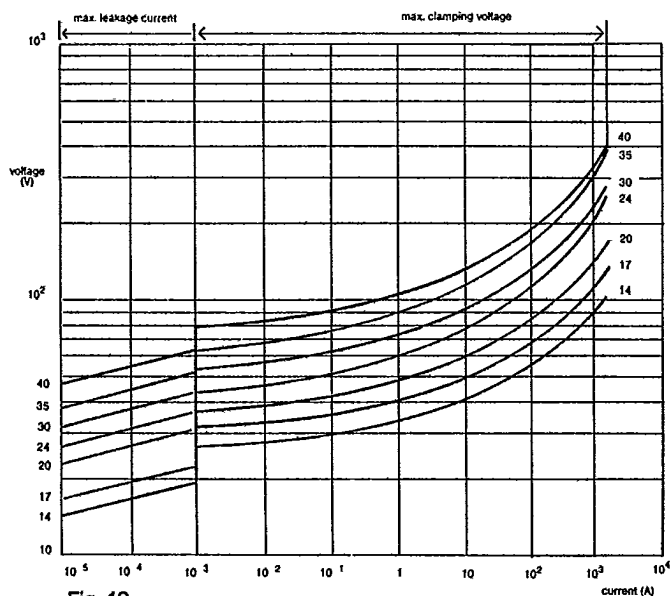


Fig. 19  
V-I characteristics, 596 series, 14 to 40 V

### 596 SERIES (B)

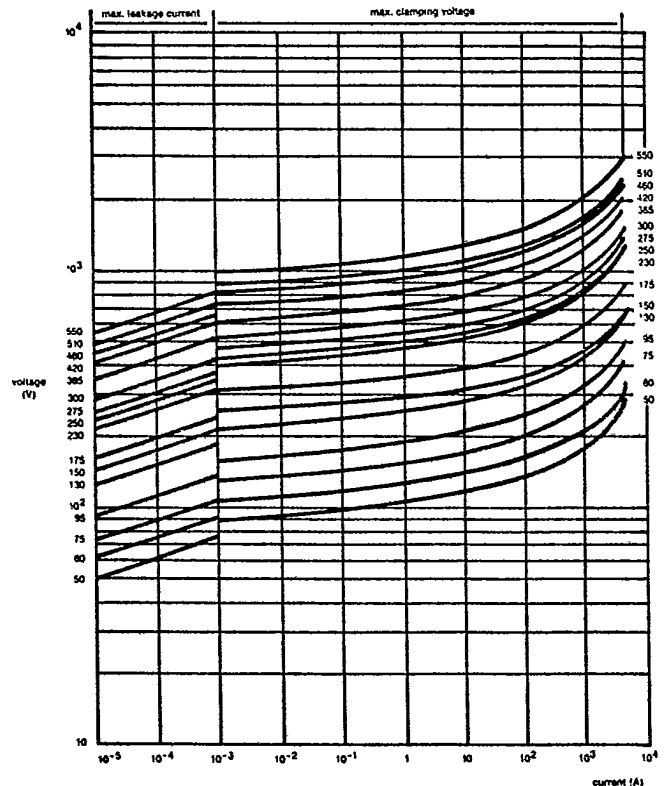


Fig. 20  
V-I characteristics, 596 series, 50 to 550 V

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# METAL OXIDE VARISTORS

## Zinc Oxide Disc

### MAX. APPLICABLE TRANSIENT CURRENT AS A FUNCTION OF IMPULSE DURATION

592 SERIES (A)

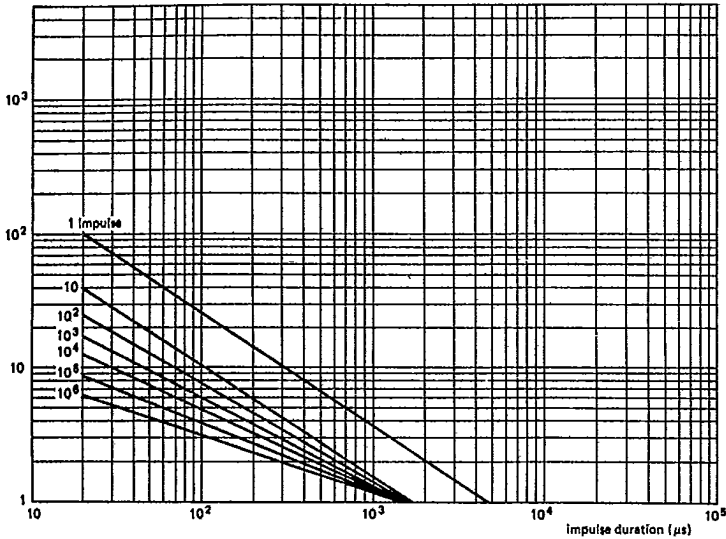


Fig. 21 Max. applicable transient current as a function of impulse duration, 592 series, 14 to 40 V

592 SERIES (B)

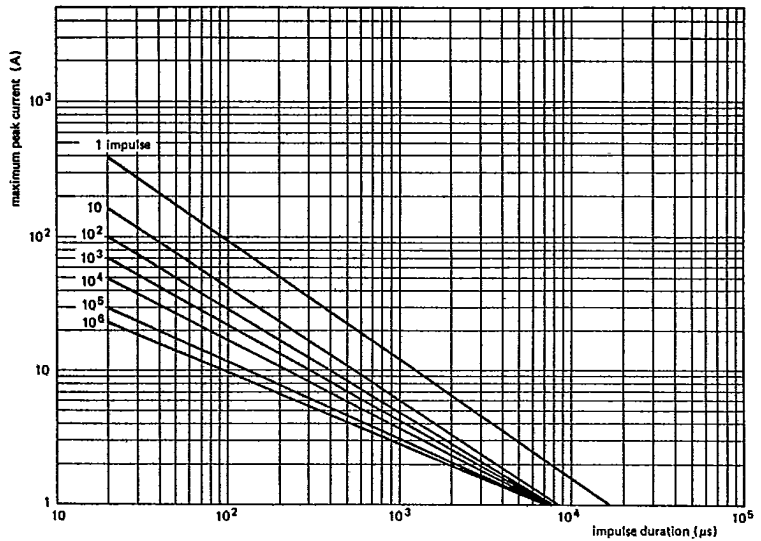


Fig. 22 Max. applicable transient current as a function of impulse duration, 592 series, 50 to 460 V

593 SERIES (A)

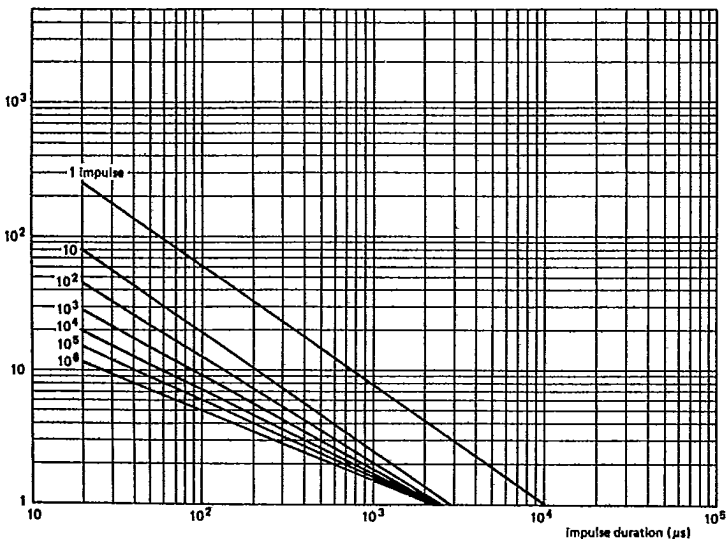


Fig. 23 Max. applicable transient current as a function of impulse duration, 593 series, 14 to 40 V

593 SERIES (B)

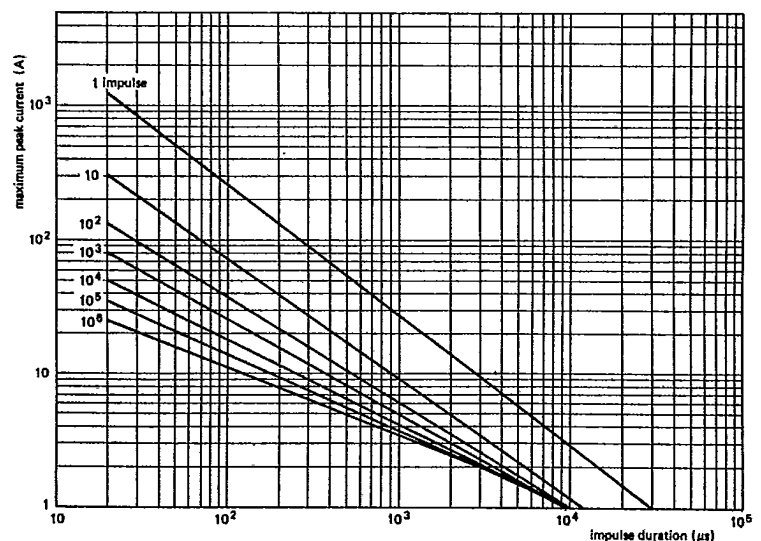


Fig. 24 Max. applicable transient current as a function of impulse duration, 593 series, 50 to 460 V



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# METAL OXIDE VARISTORS

## Zinc Oxide Disc

### MAX. APPLICABLE TRANSIENT CURRENT AS A FUNCTION OF IMPULSE DURATION

#### 594 SERIES (A)

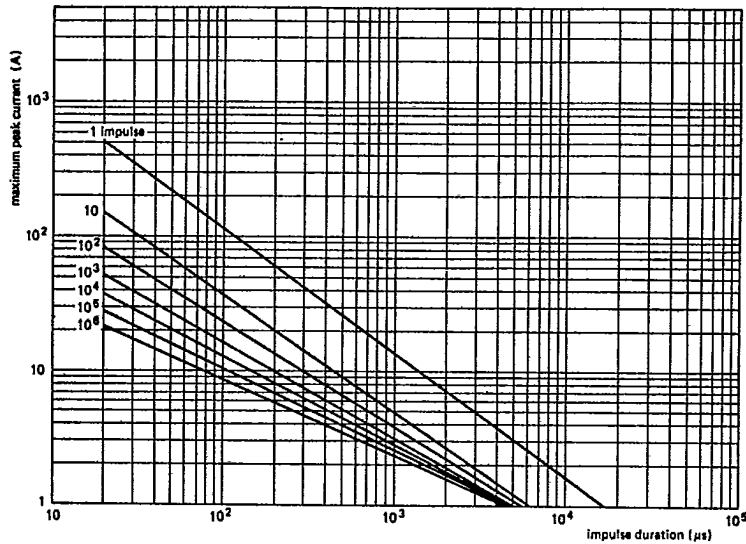


Fig. 25 Max. applicable transient current as a function of impulse duration, 594 series, 14 to 40 V

#### 594 SERIES (B)

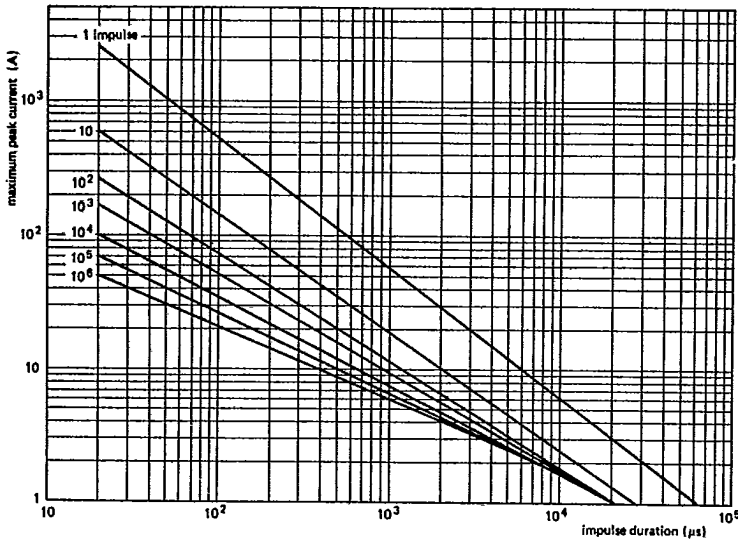


Fig. 26 Max. applicable transient current as a function of impulse duration, 594 series, 50 to 550 V

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# METAL OXIDE VARISTORS

## Zinc Oxide Disc

### MAX. APPLICABLE TRANSIENT CURRENT AS A FUNCTION OF IMPULSE DURATION

595 SERIES (A)

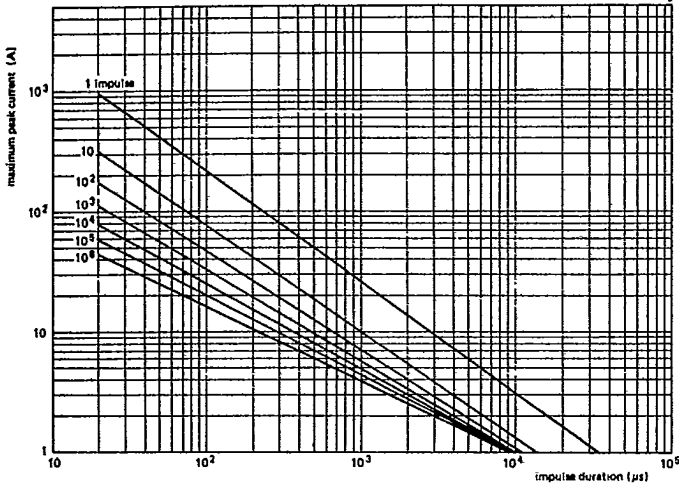


Fig. 27 Max. applicable transient current as a function of impulse duration, 595 series, 14 to 40 V

595 SERIES (B)

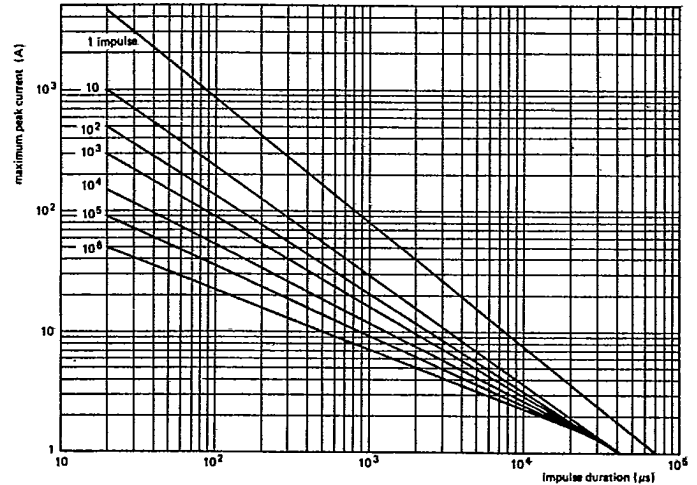


Fig. 28 Max. applicable transient current as a function of impulse duration, 595 series, 50 to 550 V

596 SERIES (A)

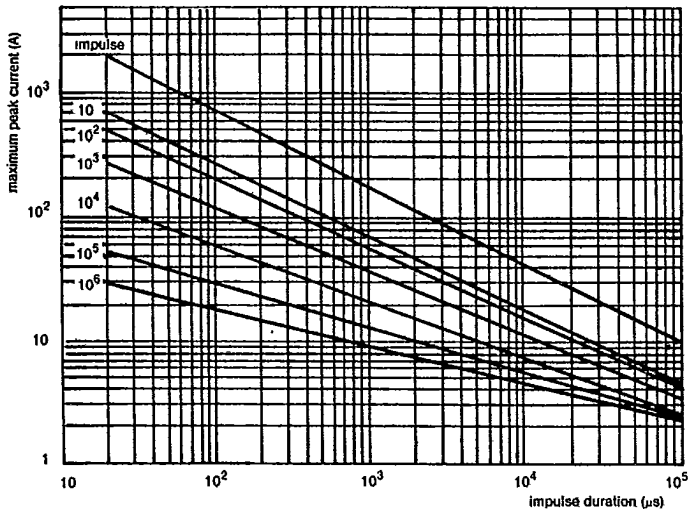


Fig. 29 Max. applicable transient current as a function of impulse duration, 596 series, 14 to 40V

596 SERIES (B)

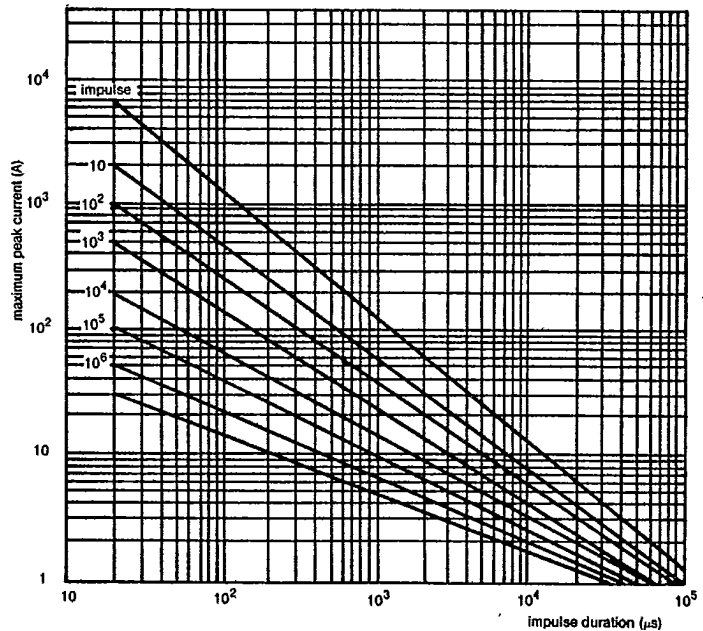


Fig. 30 Max. applicable transient current as a function of impulse duration, 596 series, 50 to 550V



# METAL OXIDE VARISTORS

## Zinc Oxide Disc

### VOLTAGE

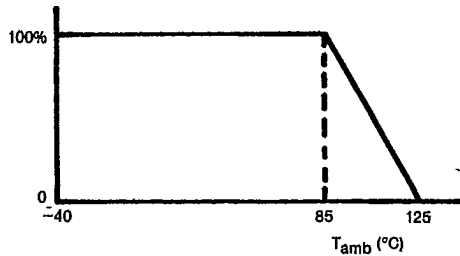


Fig. 31 Derating of max. DC or RMS working voltage with temperature.

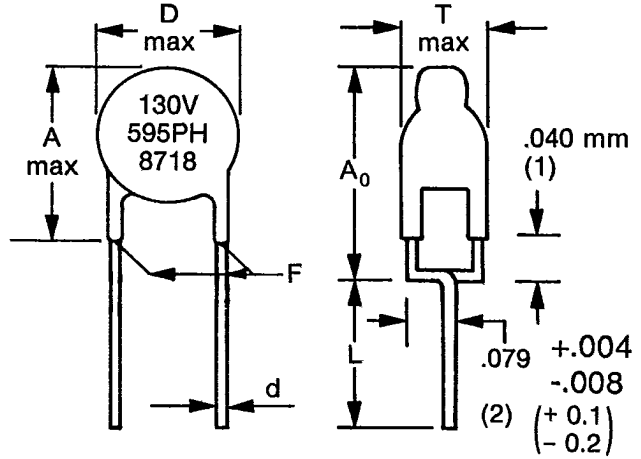


Figure 32B Kinked Lead

### MECHANICAL DIMENSIONS:

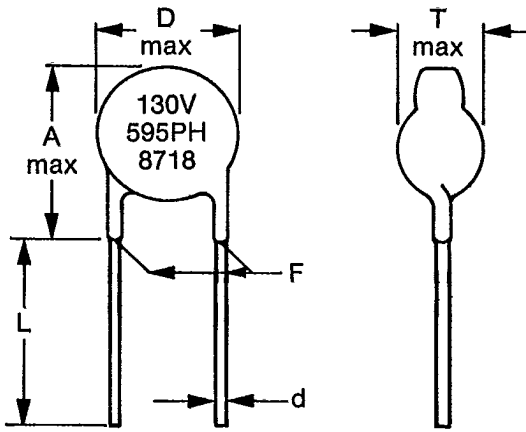


Figure 32A Straight Lead

Table 3 Maximum thickness (T) in inches (mm) from Table 2

RMS VOLTAGE	SERIES 592, 593	SERIES 594, 595, 596
14-95	0.162 (4.1)	0.173 (4.4)
130	0.165 (4.2)	0.181 (4.6)
140-150	0.173 (4.4)	0.189 (4.8)
175	0.181 (4.6)	0.197 (5.0)
230-275	0.193 (4.9)	0.213 (5.4)
300	0.209 (5.3)	0.232 (5.9)
320-385	0.228 (5.8)	0.260 (6.6)
420	0.232 (5.9)	0.260 (6.6)
460	0.236 (6.0)	0.260 (6.6)
510	—	0.272 (6.9)
550	—	0.276 (7.0)

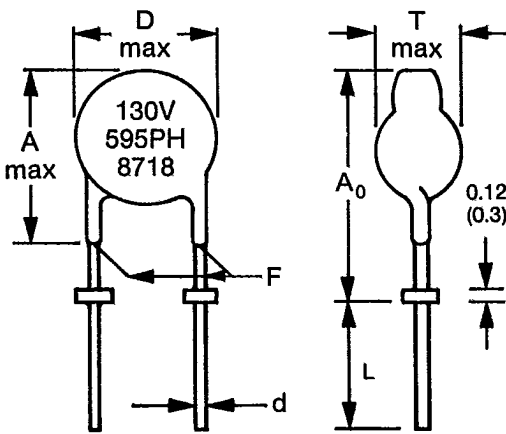


Figure 32C Flanged Lead

Table 2 Dimensions in inches (mm) for Figures 32A, B, C

SERIES	D (MAX)	T (MAX)	A (MAX)	L (MIN)	D (±10%)	F	A (MAX)
592	0.276 (7)	0.236 (6.0)	0.355 (9)	0.787 (20)	0.024 (0.6)	0.197 +0.315 -0.008 (5) (+0.8) (-0.2)	0.433 (11)
593	0.354 (9)	0.236 (6.0)	0.433 (11)	0.748 (19)	0.024 (0.6)	0.197 +0.315 -0.008 (5) (+0.8) (-0.2)	0.512 (13)
594	0.531 (13.5)	0.276 (7.0)	0.610 (15.5)	0.669 (17)	0.032 (0.8)	0.300 ±0.039 (7.62) (±1)	—
595	0.669 (17)	0.276 (7.0)	0.748 (19)	0.630 (16)	0.032 (0.8)	0.300 ±0.039 (7.62) (±1)	—
596	0.945 (24)	0.276 (7.0)	1.004 (25.5)	1.000 (25.4)	0.032 (0.8)	0.300 ±0.039 (7.62) (±1)	—

Dimension 'T' dependent on RMS Voltage rating (see Table 3)

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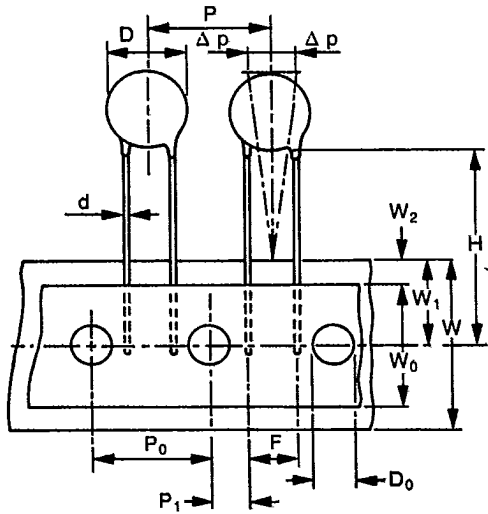


Fig. 33 Straight Lead

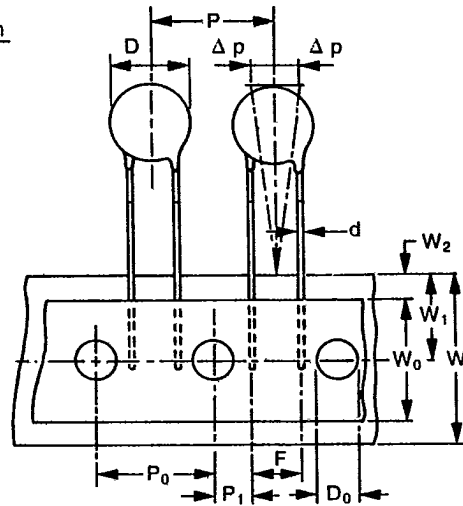
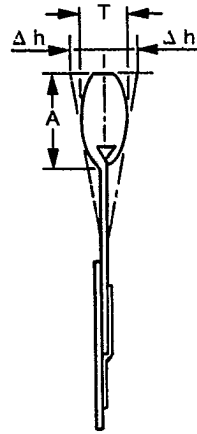


Fig. 33C Flanged Lead

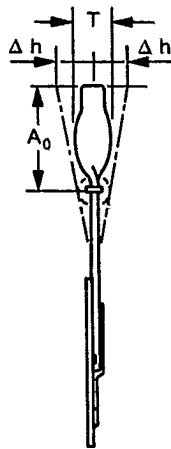


Fig. 33B Kinked Lead

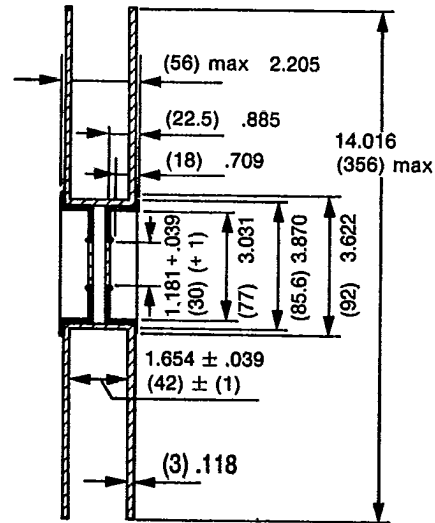
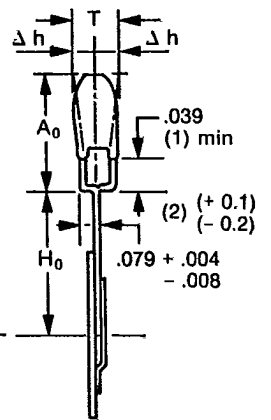


Fig. 33D Reel Dimensions



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Table 4. Dimensions in inches (mm) for Figures 33A, B, C

Dimensional Data				
Details	Symbol	Dimensions Nominal	Tolerance	Remarks
Body diameter	D	see table 2		
Total thickness	T	see table 3		
Mounting height	A <sub>0</sub> -A	see table 2		
Lead wire diameter	d	see table 2		
Pitch of components	P	(12.7) .500	(±1) ±.040	
Feed hole pitch	P <sub>0</sub>	(12.7) .500	(±0.3) ±.012	cumulative pitch error (±1 mm) 20 pitches
Feed hole centre to lead centre	P <sub>1</sub>	(3.81) .150	(±0.7) ±.028	guaranteed between component and tape
Component alignment	Δp	0	(±1.3) ±.051	
Lead to lead distance	F	see table 2		guaranteed between component and tape
Component alignment	Δh	(0) 0	(±2) ±.079	
Tape width	W	(18) .709	(+1/-0.5) +.039/-0.020	
Hold down tape width	W <sub>0</sub>	.492 (12.5) min.		
Hole position	W <sub>1</sub>	(9) .354	(±0.5) ±.079	
Hold down tape position	W <sub>2</sub>	.118 (3) max.		
Distance component to tape centre	H	(20) .787	(+2) ±.079	
Lead wire clinch height	H <sub>0</sub>	(18.25 or 16) .719 or .630	(±0.5) ±.020	see table 5
Free hole diameter	D <sub>0</sub>	(4) .157	(±0.2) ±.008	
Total tape thickness	t	(0.9 max.) .035		with cardboarded tape (0.5±0.1) .020±.004
AQL: mechanical	Level II		1%	

# METAL OXIDE VARISTORS

Table 5. Packaging Configurations

Code number 2322	Packing quantity	Packing	H inches (mm) See table 4	Outline	
592-	0...6	1500	reel	.630 (16)	fig. 33A
	1...6	1500	reel		fig. 33C
	2...6	1500	reel	.719 (18.25)	fig. 33C
	3...6	1500	reel		fig. 33B
	5...6	500	bulk	—	fig. 32A
6...6	6...6	500	bulk	—	fig. 32B
	7...6	250	bulk		fig. 32C
8...6	1500	reel	.630 (16)	fig. 33B	
593-	0...6	1500	reel	—	fig. 33A
	1...6	1500	reel		.630 (16)
	2...6	1500	reel	.719 (18.25)	fig. 33C
	3...6	1500	reel		fig. 33B
	5...6	500	bulk	—	fig. 32A
6...6	6...6	500	bulk	—	fig. 32B
	7...6	250	bulk		fig. 32C
8...6	1500	reel	.630 (16)	fig. 33B	
594-	0...6	7501	reel	—	fig. 33A
	5...6	250	bulk		fig. 32A
595-	03006 to 01716	7501	reel	—	fig. 33A
	53006 to 51716	250	bulk		fig. 32A
	02316 to 05516	7501	reel	—	fig. 33A
52316 to 55516	100	bulk	fig. 32A		
596-	5...6	50	bulk	—	fig. 33A

Table 6. Metal Oxide Varistor Part Number Definition

**2322**

Philips  
Product

**592**

Varistor  
Disc Size  
592 = 5 mm  
593 = 7 mm  
594 = 10 mm  
595 = 14 mm  
596 = 20 mm

**5**

\*Packaging/Lead Type  
0 = T & R/Straight  
1,2 = T & R/Flange †  
3,8 = T & R/Kinked †  
5 = Bulk/Straight  
6 = Bulk/Kinked  
7 = Bulk/Flange

\* Series 594, 595 are only available as type 0 and 5

\*Series 596 only available as type 5

†See Tape and Reel Dimensions

**750**

Maximum Continuous  
RMS Voltage

140 = 14V	750 = 75V	301 = 300V
170 = 17V	950 = 95V	321 = 320V
200 = 20V	131 = 130V	381 = 385V
250 = 25V	141 = 140V	421 = 420V
300 = 30V	151 = 150V	461 = 460V
350 = 35V	171 = 175V	511 = 510V
400 = 40V	231 = 230V	551 = 550V
500 = 50V	251 = 250V	
600 = 60V	271 = 275V	

**6**

Ochre  
Epoxy Coating

6 = Ochre Epoxy Coating  
\*\*7 = Ammo Pack Tape &  
Ochre Epoxy Coating

\*\*Only available for 592 & 593 Series



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**Table 7. Test Results**

**Notes** 1. Clause numbers of tests and performance requirements refer to CECC 42000

2. Inspection levels and AQL's are selected from IEC Publication 410.

3. In this table: p = periodicity (in months)

n = sample size

c = acceptance criterion (permitted number of defectives)

D = destructive

ND = non-destructive

4. The varistors shall be mounted by their normal means in such a manner that there shall be no parasitic vibration.

Clause number and test (see note 1)	D or ND	Conditions of test (see note 1)	IL	AQL (see note 2)	Performance requirements (see note 1)
<b>GROUP A INSPECTION</b> (lot-by-lot) <b>Sub-Group A1</b> 4.2.1. Visual examination 4.2.2. Marking	ND			1.0%	As in 4.2.1. As in 4.2.2.
<b>Sub-Group A2</b> B2.6 Protection level 4.3. Voltage	ND	At class current given in table 2 At 1 mA		0.65%	As specified in table 2 Values given in table 2
<b>Sub-Group A3</b> 4.2.3. Dimensions (gauging)	ND	D and T		1.0%	As specified in tables 1 and 2
<b>GROUP B INSPECTION</b> (lot-by-lot) <b>Sub-Group B1</b> 4.11. Robustness of terminations  4.10.1. Solderability  x.x. Solvent resistance of coating and marking	D	Test Ua and Ub of IEC 68-2-21 Visual examination Voltage at 1 mA Solder bath method: 235±5°C Visual examination IEC 68-2-45 (1980) Test Xa Solvent: 3.1.1. Temperature: 23±5°C		2.5%	As in 4.11.6. Within the values given in table 2 The terminations shall be uniformly tinned No visual damage Legible marking
<b>Sub-Group B2</b> 4.7. Voltage proof	D	Method: metal balls (4.7.1.2.) 2500 V		1.0%	As in 4.7.3.

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Clause number and test (see note 1)	D or ND	Conditions of test (see note 1)	Sample size and criterion of acceptability			Performance requirements (see note 1)
			(see note 3)			
			p	n	c	
<b>GROUP C INSPECTION</b> (periodic) <b>Sub-Group C1</b> x.y. Maximum surge current	D	100 pulses 8/20 $\mu$ s at 2 per min in one direction Visual examination Voltage at 1 mA	6	13	1	No visible damage $\Delta V/V: \pm 10\%$ max.
<b>Sub-Group C2</b> x.z. Maximum peak current	D	100 pulses 10/1000 $\mu$ s in one direction, 1 every 2 min Visual examination Voltage at 1 mA	12	13	1	No visible damage $\Delta V/V: \pm 10\%$ max.
<b>Sub-Group C3</b>  4.6. Capacitance  4.10.2. Resistance to soldering heat  4.12. Rapid change of temperature  4.14. Shock  4.17. Climatic sequence - Dry heat - Damp heat, cyclic, first cycle - Cold - Damp heat, cyclic, remaining cycles - Final measurement	D	<b>7 specimens</b> f = 1 kHz Signal level 1 V max Zero bias Method Tb of IEC 68-2-20A Visual examination Voltage at 1 mA Test Na of IEC 68-2-14 Ta: Lower category temp.: -40°C Tb: Upper category temp.: 125°C Visual examination Voltage at 1 mA <b>6 specimens</b> Pulse shape: half sine Acceleration: 490 m/s <sup>2</sup> Pulse duration: 11 ms 3 x 6 shocks Visual examination Voltage at 1 mA <b>All specimens</b>  Visual examination Voltage at 1 mA Voltage proof	12	13	1	As given in table 2 with $\pm 50\%$  As in 4.10.2.4. $\Delta V/V: \pm 5\%$ max.  As in 4.12.4 $\Delta V/V: \pm 5\%$ max.  As in 4.14.3 $\Delta V/V: \pm 5\%$ max.  As in 4.16.9.1 $\Delta V/V: \pm 5\%$ max. As in 4.7.3.



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Clause number and test (see note 1)	D or ND	Conditions of test (see note 1)	Sample size and criterion of acceptability (see note 3)			Performance requirements (see note 1)
			p	n	c	
<b>Sub-Group C4</b> 4.20. Endurance at upper category temperature	D	1000 h at 85°C and at max. r.m.s. voltage Examination at 48 h, 500 h and 1000 h Visual examination Voltage at 1 mA Examination at 1000 h Voltage at class current Voltage proof	12	13	1	As in 4.20.5.1. $\Delta V/V: \pm 5\%$ max. 1,1 x the initial limits As in 4.7.3.
<b>GROUP D INSPECTION</b> (periodic) <b>Sub-Group D1</b> 4.17. Damp heat, steady state	D	<b>4 specimens</b> No applied voltage <b>Other 4 specimens</b> Applied voltage: 10% of the max. d.c. voltage Visual examination Voltage at 1 mA Voltage proof	24	8	1	As in 4.17.3.1. $\Delta V/V: \pm 5\%$ max. As in 4.7.3.
<b>Sub-Group D2</b> 4.2. Dimensions (detail) 4.5. Temperature coefficient of voltage	ND	At 1 mA	24	8	1	As specified in table 1 and 2 -0.065%/°C
<b>Sub-Group D3</b> 4.18. Inflammability Needle flame test	D	Test IEC 695-2-2 10 s—vertical	24	5	0	5 s max.

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